

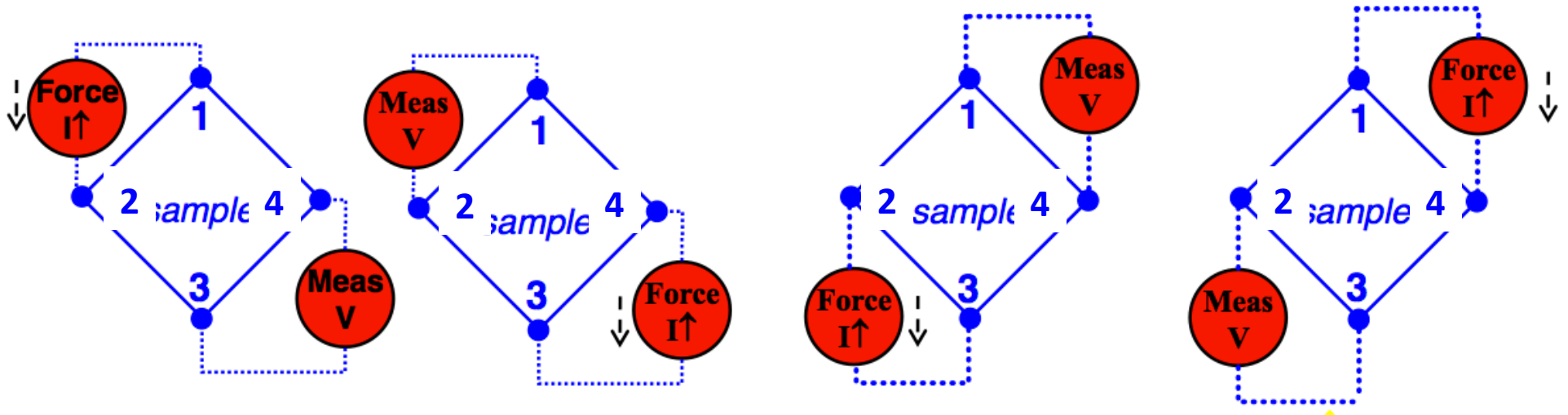
# Hall Effect Measurements

## Practical Issues

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JMR 10/28/14

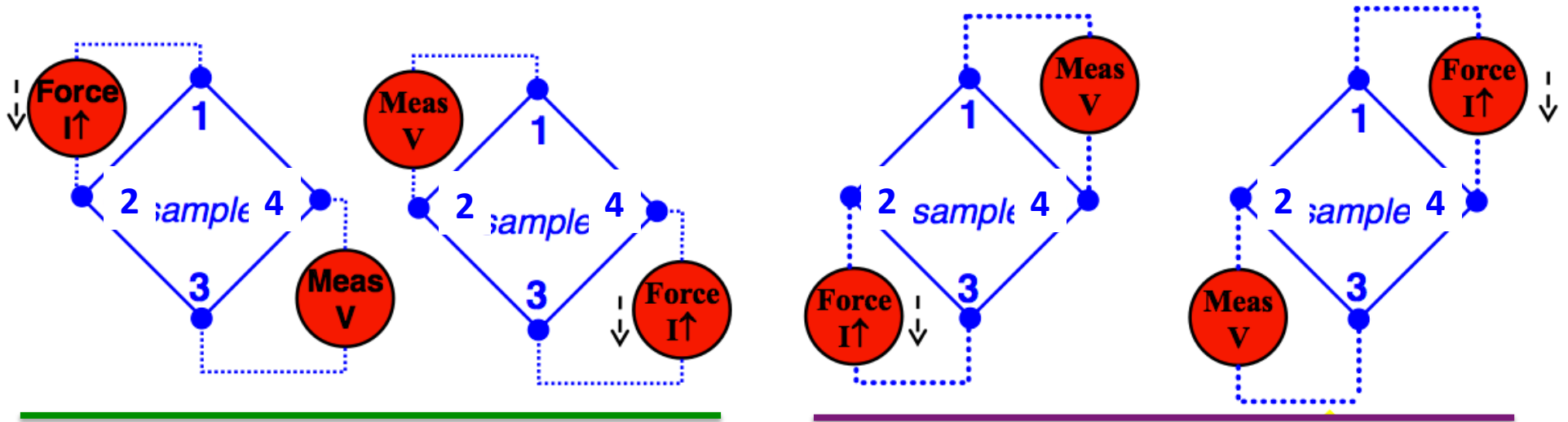
# Basics – van der Pauw resistivity



Best results for

- uniform sample
- high symmetry
- point contacts (for blanket coat)
- Ohmic contacts
- low contact resistance

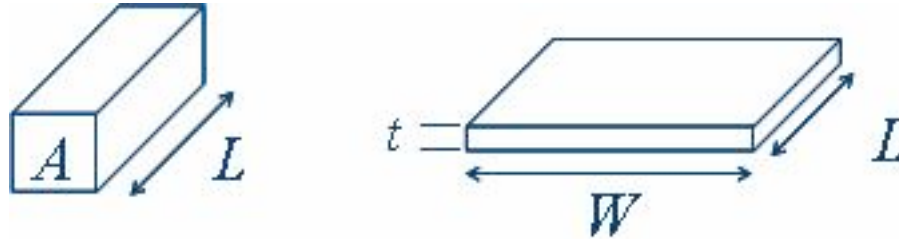
# Basics – van der Pauw resistivity



$$e^{-\pi R_A / R_{sheet}} + e^{-\pi R_B / R_{sheet}} = 1$$

$$\rho = R_{sheet} t$$

# Aside – sheet resistance

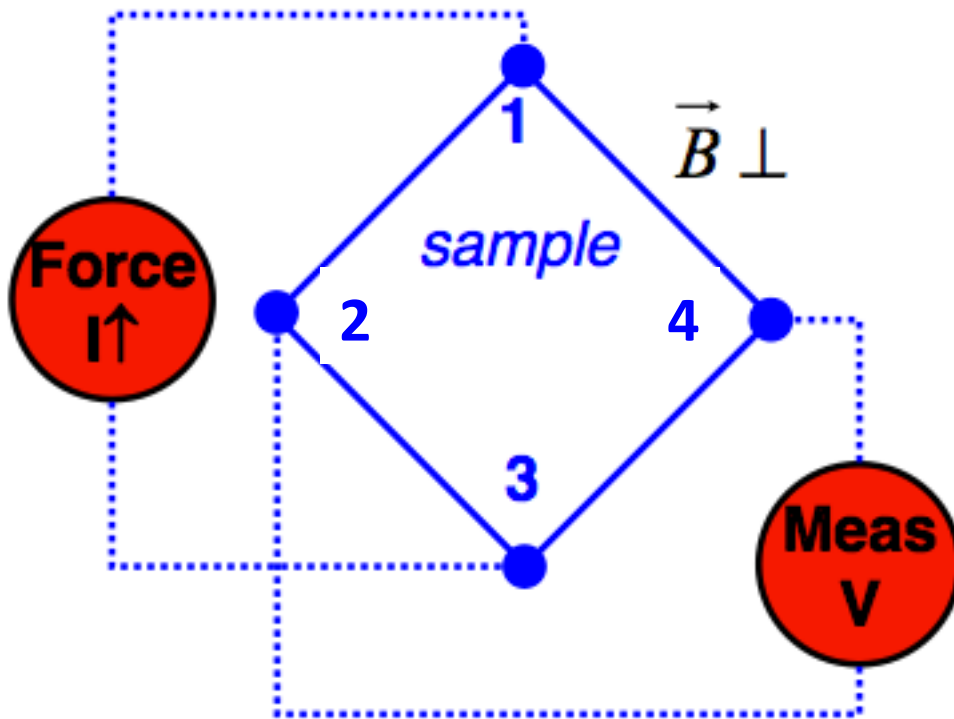


$$R = \rho \frac{L}{Wt} = \frac{\rho}{t} \frac{L}{W} \equiv R_{sheet} \frac{L}{W}$$

$$R_{sheet} = \frac{\rho}{t}$$

Dimensions of  $\Omega$ , but really  $\Omega \text{ cm/cm}$

# Basics - van der Pauw Hall

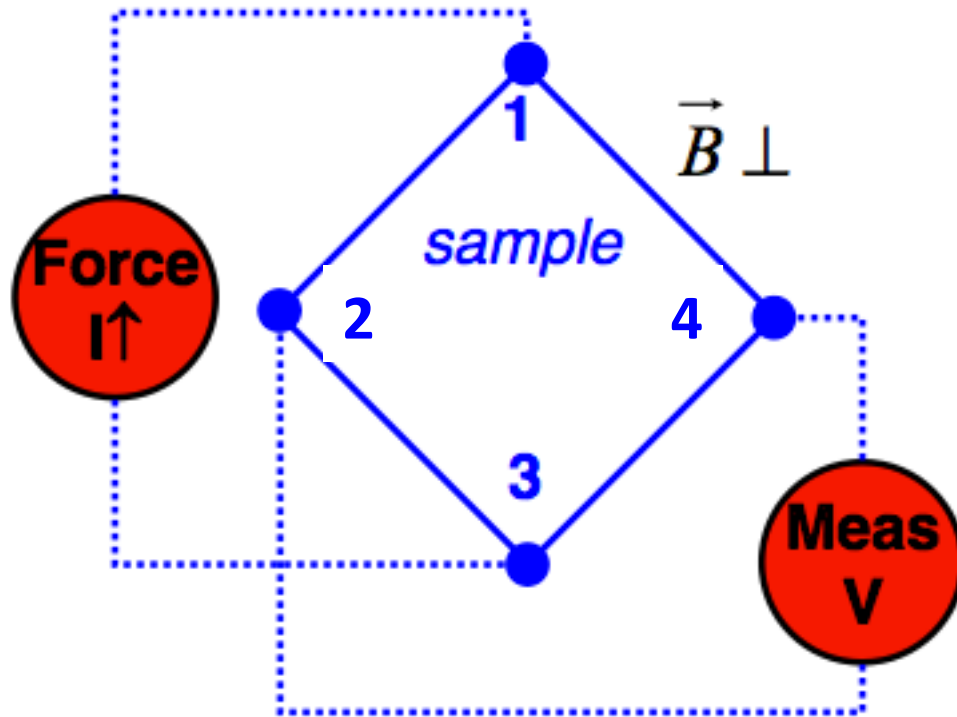


Apply I, measure  $V_+$ ,  $V_-$   
Reverse I, measure  $V_+$ ,  $V_-$   
Apply I to 2 & 4, repeat  
Reverse B field and repeat

**TIME** to reverse B !

- Instrument drift
- Temperature drift
- Change temperature gradients

# Basics - van der Pauw Hall



$$R_H = \frac{r}{q(n-p)}$$

$$R_{HA} = 10^8 \frac{t}{B} \left[ \frac{V_{31,42}^{+/+} - V_{31,42}^{-/+} + V_{31,42}^{-/-} - V_{31,42}^{+/-}}{I_{31}^{+/+} - I_{31}^{-/+} + I_{31}^{-/-} - I_{31}^{+/-}} \right] \text{cm}^3 \text{C}^{-1}$$

# All the other effects ....

**Table A-2** Hall effect measurement voltages showing the elimination of all but the Hall and Ettingshausen voltages by combining readings with different current and magnetic field polarities.

	I	B	$V_H$	$V_M$	$V_S$	$V_E$	$V_N$	$V_R$	$V_O$
$V_1$	+	+	+	+	+	+	+	+	+
$V_2$	-	+	-	-	+	-	+	+	+
$(V_1 - V_2)$			$2V_H$	$-2V_M$	0	$2V_E$	0	0	0
$V_3$	+	-	-	+	+	-	-	-	+
$V_4$	-	-	+	-	+	+	-	-	+
$(-V_3 + V_4)$			$2V_H$	$-2V_M$	0	$2V_E$	0	0	0
$(V_1 - V_2 - V_3 + V_4)$			$4V_H$	0	0	$4V_E$	0	0	0

$V_o$  Voltmeter offset (there is also current meter offset)

$V_s$  Seebeck voltage due to trans temp gradient

$V_e$  Ettinghausen due to internal Seebeck by  $ev \times B$  force shunting slow (cool) and fast (hot) electrons to the sides in different numbers

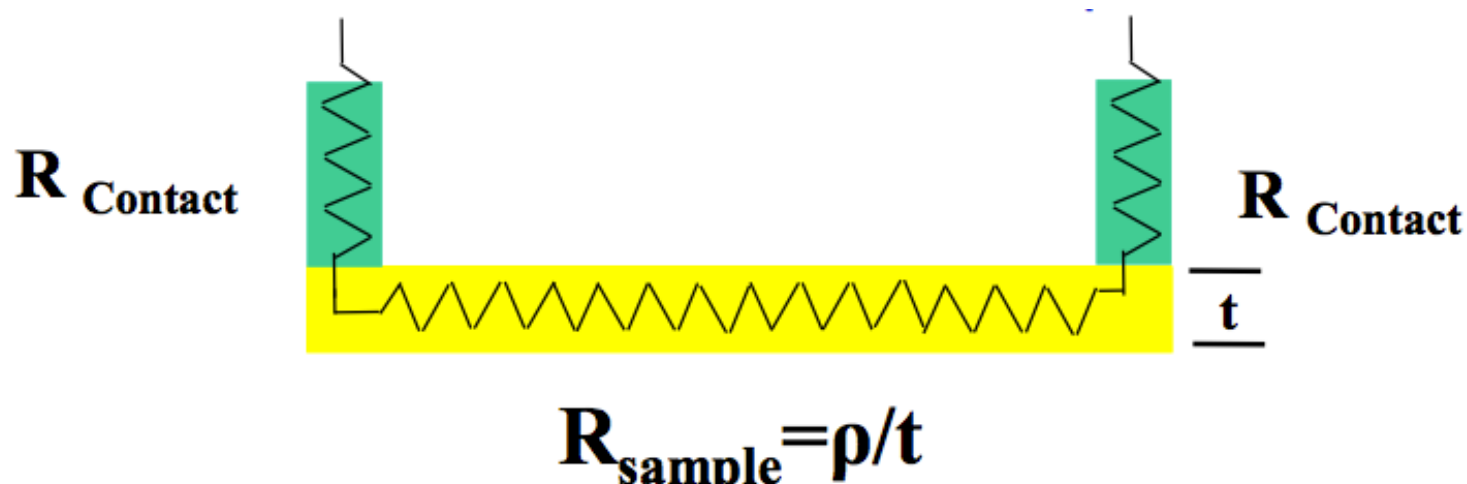
$V_n$  Nernst due to long temp gradient – causes current that generates Hall voltage in B

$V_r$  Righi-Luduc – Ettinghausen of the thermally generated current

$V_m$  misalignment

# Resistance ranges

- Total Resistance = Sample R + Contact R
- Sample  $R = \rho/t$  (*square sample*); sample resistivity  $\rho$ , thickness  $t$ . Limits total current. Try to keep power dissipation 1-5 mW
- Contact R at metal semiconductor interface (nominal)  
GaAs  $\sim 1000 * R_{\text{sample}}$ ; Si:  $\sim 300 * R_{\text{sample}}$





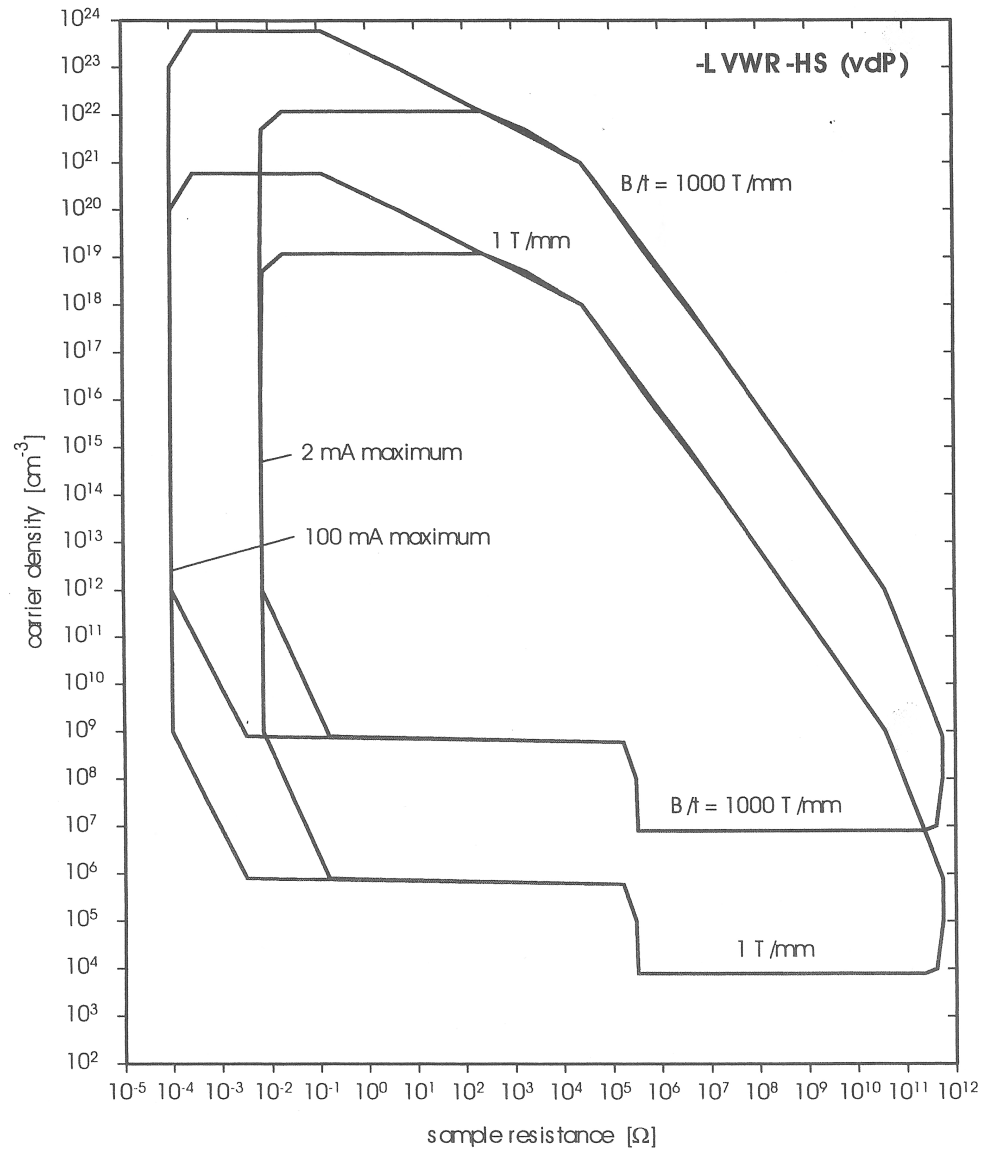
# Resistance ranges

- Mid range resistance

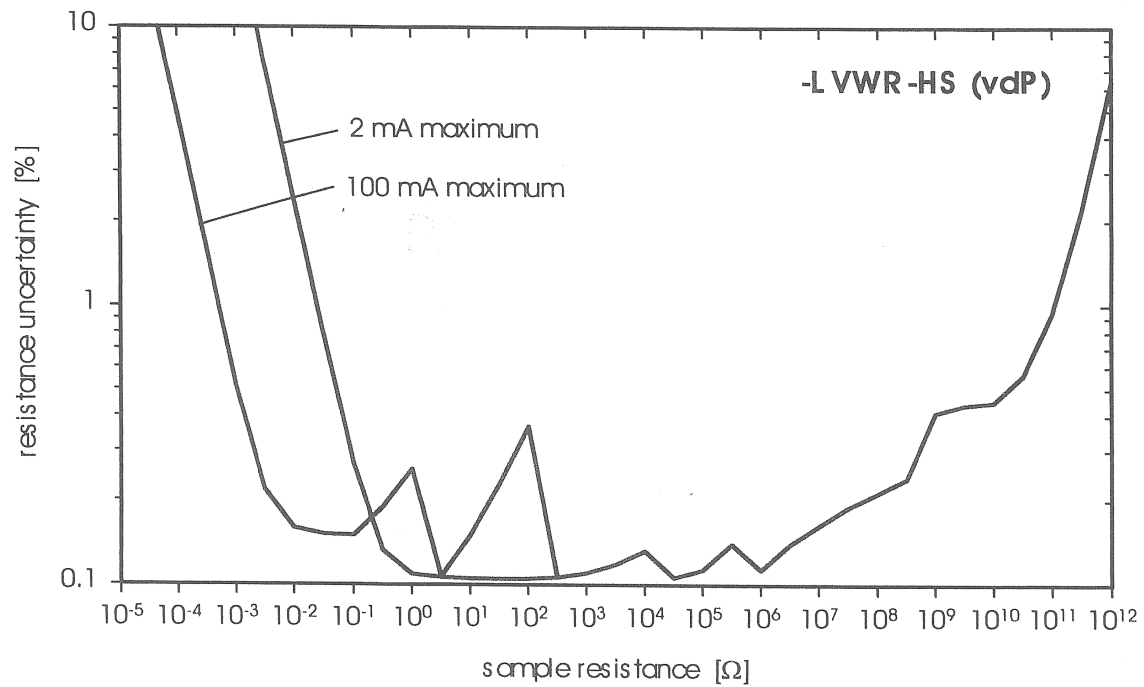
100 m $\Omega$  to 1 M $\Omega$

Typically: Nominally doped Si or Ge

( $\sim 10^{15} \text{cm}^{-3}$ ); Si photovoltaics; pHEMTs; ITO



**Figure 1-18** Range within which mobility is measured to within an uncertainty of 5% using the -LVWR-HS measurement configuration with metered or unmetered current (2 or 100 mA maximum, respectively) and van der Pauw structures. Manual recabling is required to switch between these conditions. Modeled measurement conditions: maximum power dissipation in the sample of 1 mW, maximum excitation or sample output voltage of 8 V, indicated maximum current, 29 K sample temperature, no current leakage to sample holder, high resistance mode used for sample resistances > 100,000 Ω, 25 Ω resistance down each lead wire, assumed sample resistivity measurement voltage efficiencies ( $V_{out}/V_{in}$ ) of 0.1 for van der Pauw structures, zero Hall offset voltage, Hall factor of 1 and magnetic flux density (B) or sample thickness (t) uncertainties of 1% each. Note that the maximum carrier density is roughly proportional to the ratio B/t, so large magnetic flux density and thin samples can improve the measurement range.



**Figure 1-17** Resistance measurement uncertainty using the -LVWR-HS measurement configuration with metered or un-metered current (2 or 100 mA maximum, respectively) and van der Pauw structures. Manual recabling is required to switch between these conditions. Modeled measurement conditions: maximum power dissipation in the sample of 1 mW, maximum excitation or sample output voltage of 8 V, indicated maximum current, 295 K sample temperature, no current leakage to sample holder, high resistance mode used for sample resistances > 100,000 Ω, and 25 Ω resistance down each lead wire.

# High resistance

- Electrostatic shielding to minimize electrical interference  
Shield the DUT and all sensitive circuitry  
(**there is a metal cover – use it!**) Use shielded cabling  
Connect the shield to the low terminal of the system
- Use guarding to reduce the effects of leakage current  
Guarded current source  
Use triax cable instead of coax cable
- Allow sufficient settling time  
Source I and measure  $V(t)$  to determine settling time  
A diamond sample can take 10–15 minutes for settling

# Thermoelectric effects

- Minimize temperature fluctuations & gradients

Shield the DUT from air currents

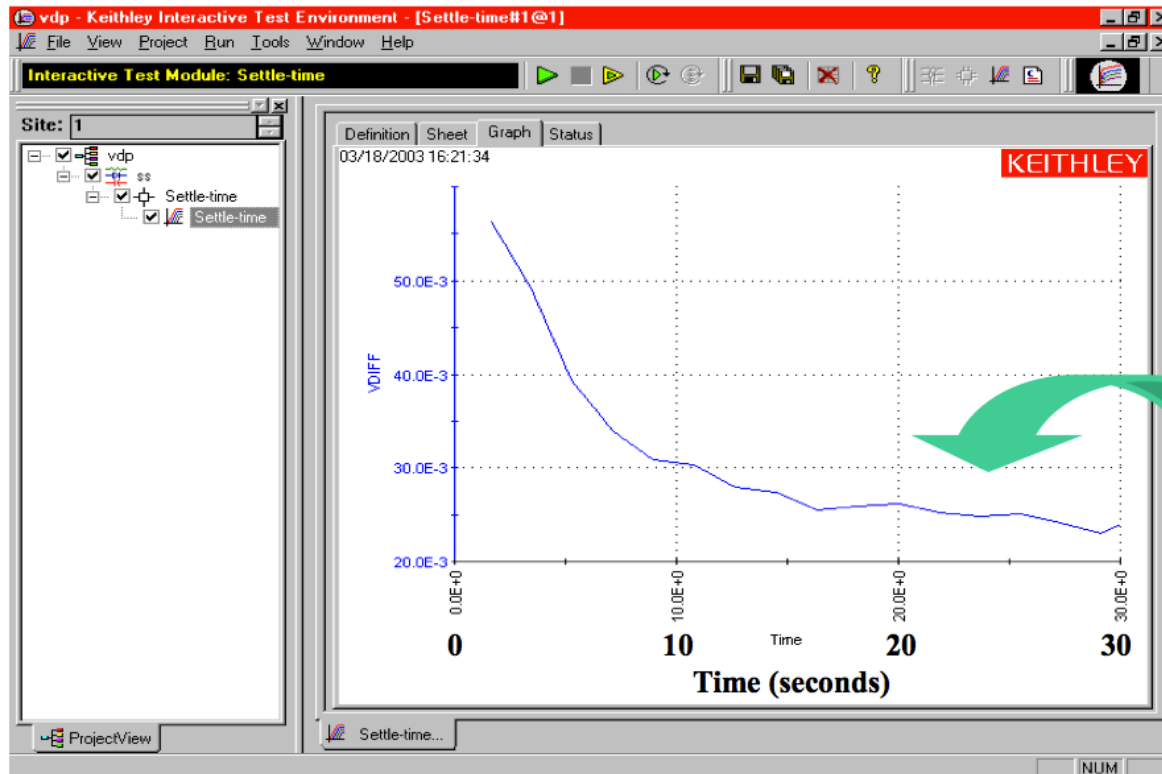
(there is a metal cover – use it!)

Keep room temperature constant 😞

Keep contacts free of oxidation

# Settling time

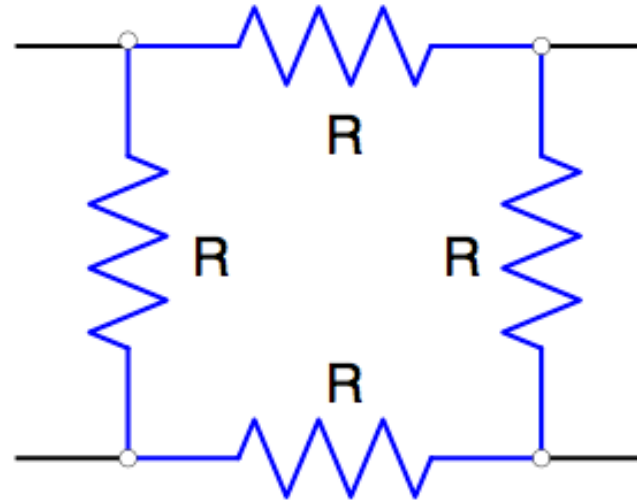
## Settling Time of a $10^{12}\Omega$ Resistance Sample



Wait at least  
20sec for a  
settled  
measurement

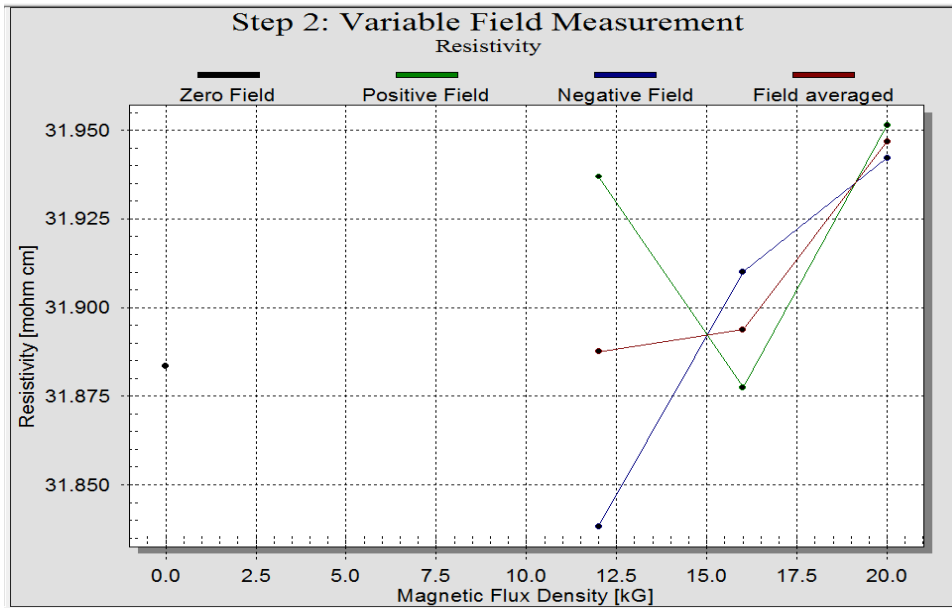
# Test and calibrate

- Test structure of four equal resistors similar in magnitude to the resistance of the sample under test



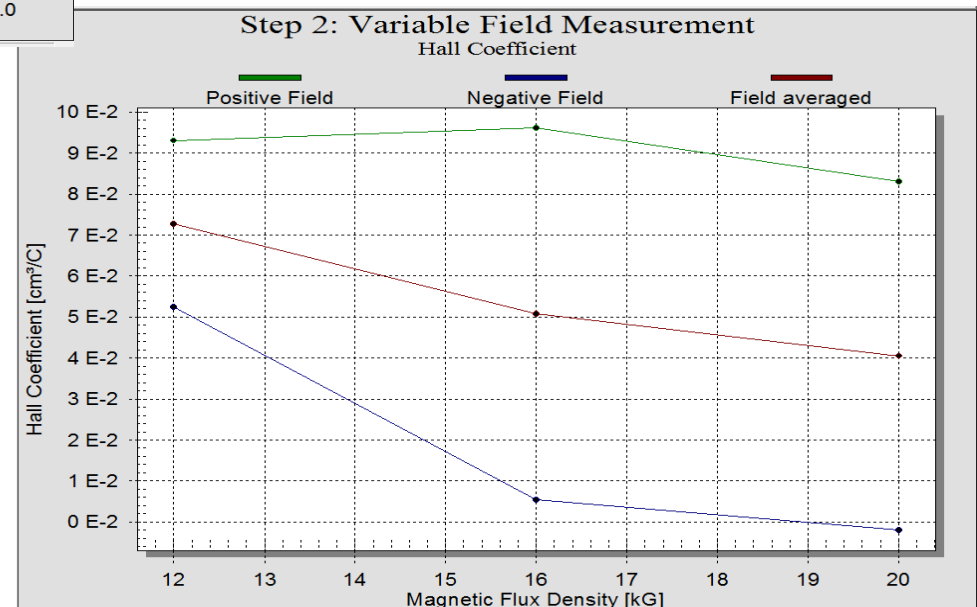
- Have a known good sample (Lakeshore provides these)
- Check the B-field measurement at “0” and other

# CATS sample (geometry was cross)



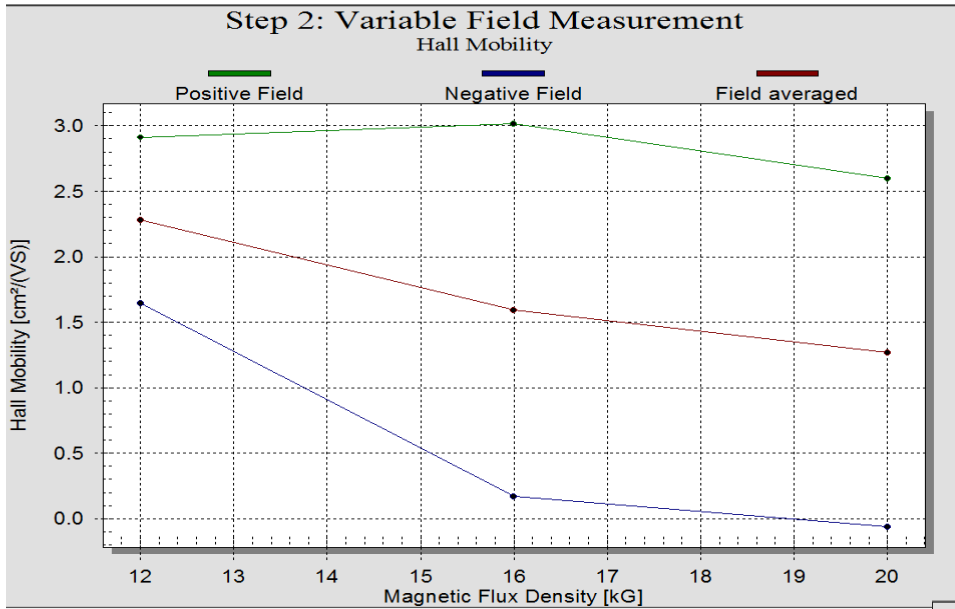
Resistivity  $\rho$  (needs  $t$ )  
 $\leftarrow$  variation 1 in 300  
 $+B/-B < 0.3\%$

Hall coefficient  $R_H$   
 variation 10 in 10  $\rightarrow$   
 $+B/-B \approx 100\%$   
 $\langle R_H \rangle = 0.5(R_{HP} + R_{HN})$





# CATS sample



Mobility =  $R_H/\rho$   
(no  $t$  needed)

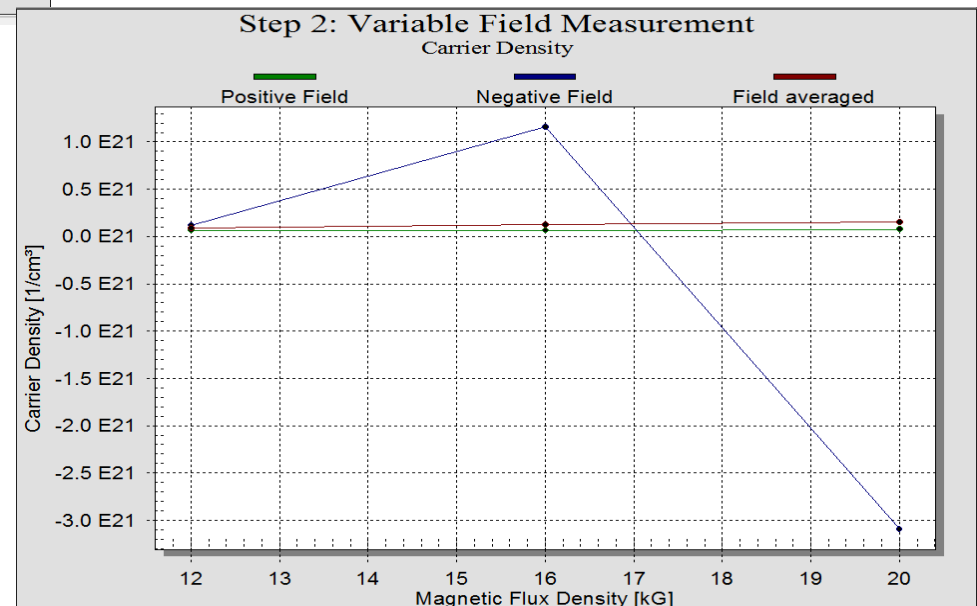
← variation 100%

Carrier density  $n$  or  $p$

variation 10 in 10 →

+B/-B ≈ 100%

$$\langle n \rangle^{-1} = n_p^{-1} + n_N^{-1}$$



# More imperfections

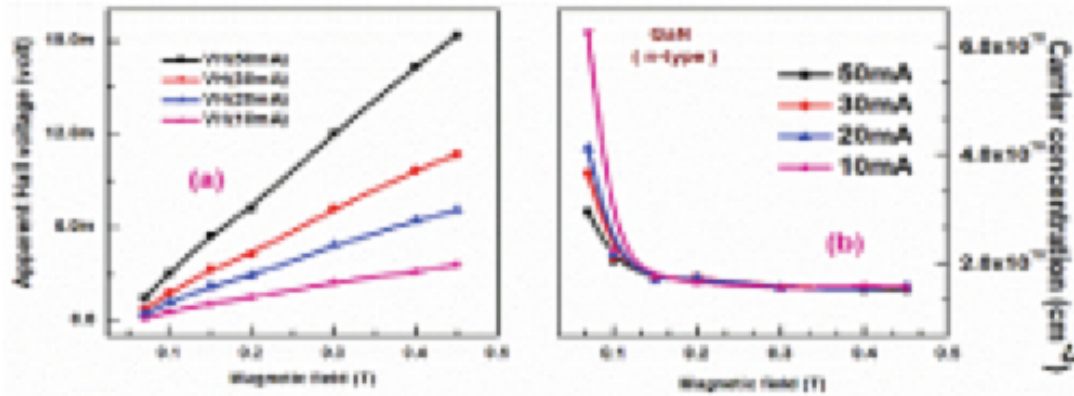


FIG. 4 (a) True Hall voltage plotted as a function of magnetic field, and (b) Carrier concentration extracted from the true Hall voltage at several current values.

$$V_H = \frac{R_H BI}{t}$$

Carrier density *seems* to vary with B – this is because the graph of  $R_H$  vs  $B$  does not properly intersect the origin – need to use slope, not absolute values (*cf*  $V=IR$  that doesn't go through origin)

# Importance of homogeneity

## Positive Hall coefficients obtained from contact misplacement on evident $n$ -type ZnO films and crystals

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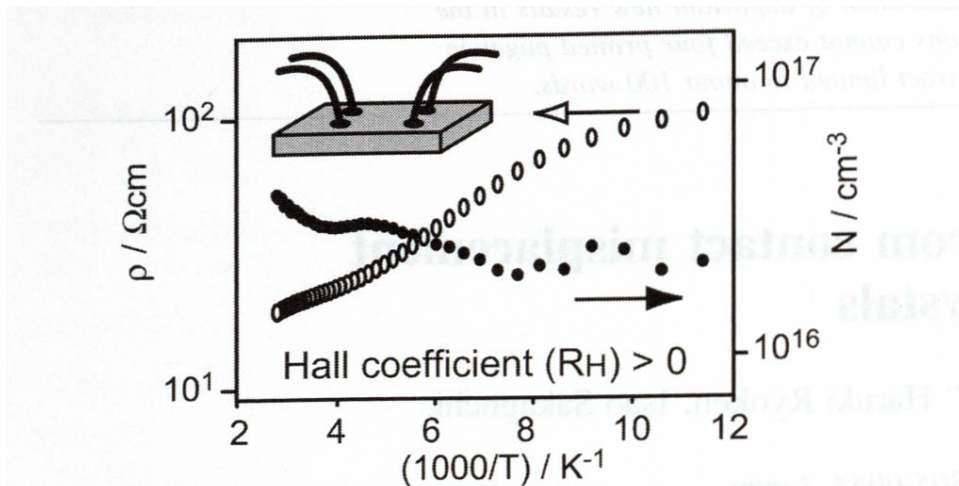


FIG. 1. Electric resistivity and “false hole concentration” in annealed ZnO single crystal.

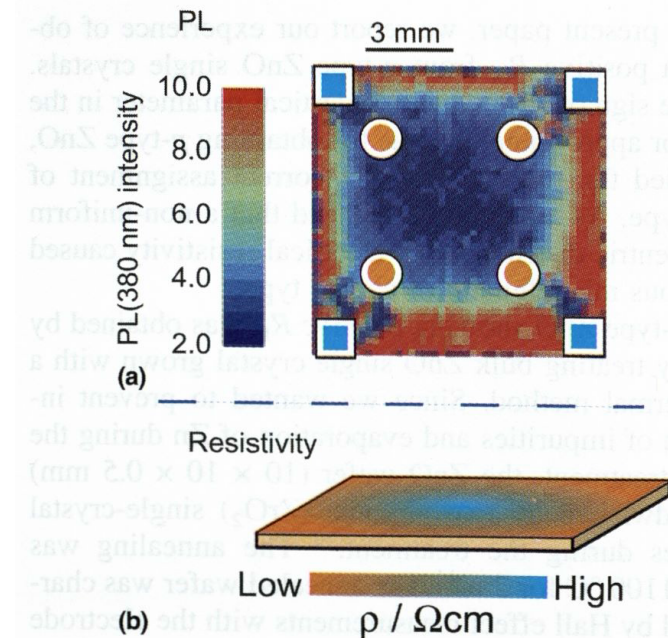


FIG. 2. (a) PL intensity mapping at  $\lambda = 380$  nm. Orange circles and blue squares indicate position of electrodes for Hall measurements (see text) and (b) speculated resistivity distribution.

# Sign reversal due to contact placement in inhomogeneous samples

- ZnO wafer treated by sandwiching between  $\text{ZrO}_2$  wafers; inhomogeneity clearly visible in PL (speculate Li impurity diffusion inhomogeneity)
- Orange contacts  $R_H > 0$
- Blue contacts  $R_H > 0$
- $F_{VdP} = 1!$  (no anisotropy in resistance measurements in either case)

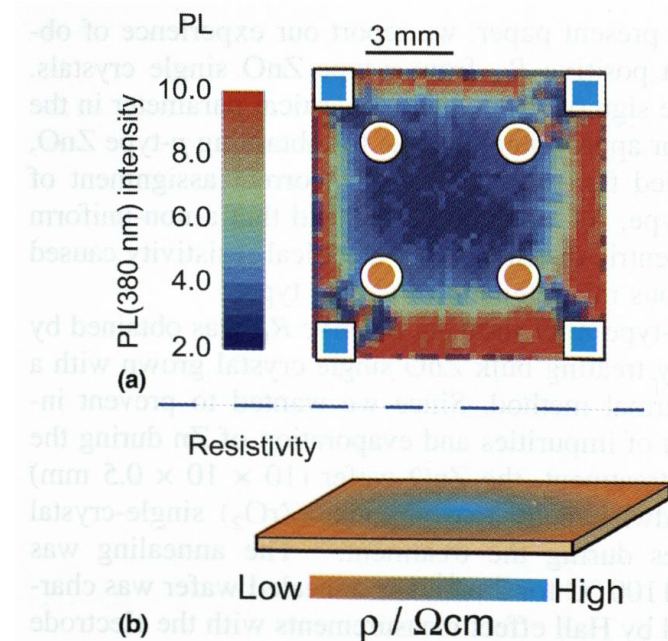


FIG. 2. (a) PL intensity mapping at  $\lambda = 380$  nm. Orange circles and blue squares indicate position of electrodes for Hall measurements (see text) and (b) speculated resistivity distribution.

# $n$ -ZnO:Al films by PLD on sapphire

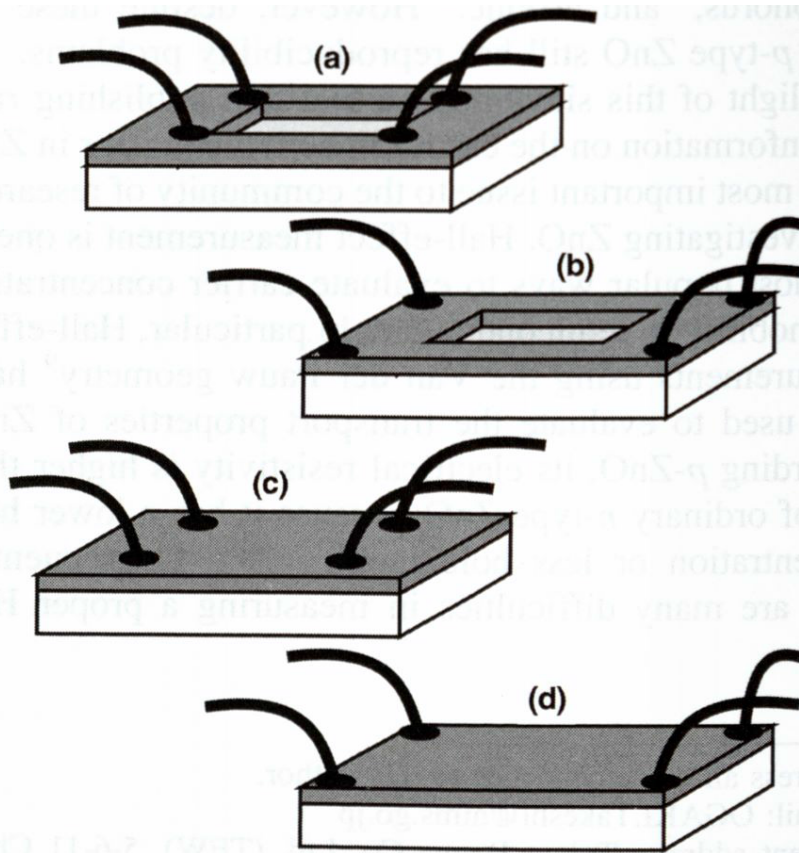


FIG. 3. Structure of ZnO samples to demonstrate Hall measurement for non-uniform samples.

(a)  $R_H > 0$

(b)  $R_H < 0$

(c)  $R_H < 0$

(d)  $R_H < 0$

- $F_{VdP} = 1$  (isotropic)

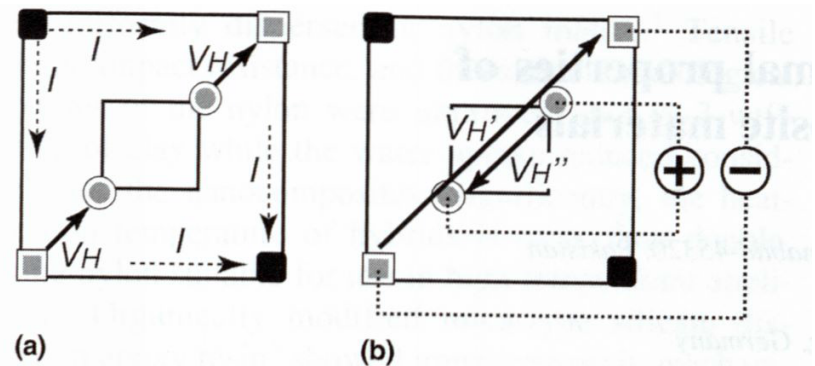


FIG. 4. Dependency of the sign of Hall coefficient on electrode configuration: (a) actual Hall voltage and (b) measured false Hall voltage.